

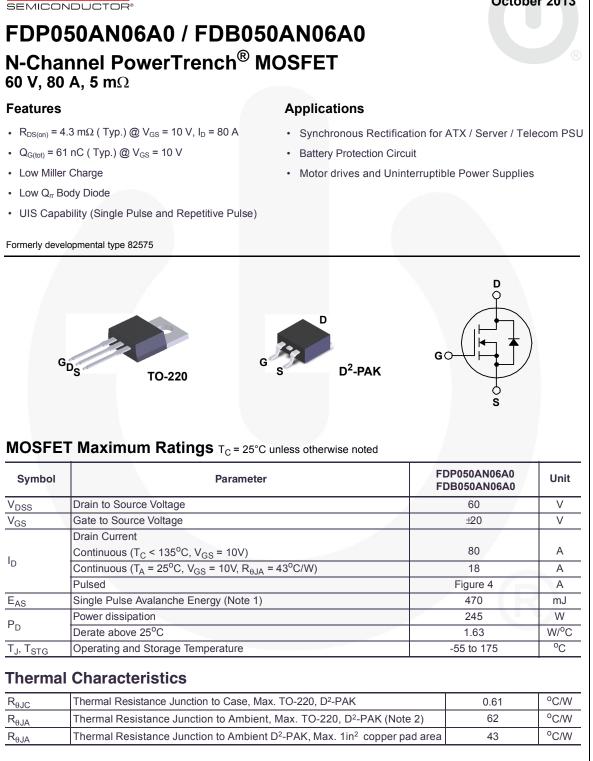
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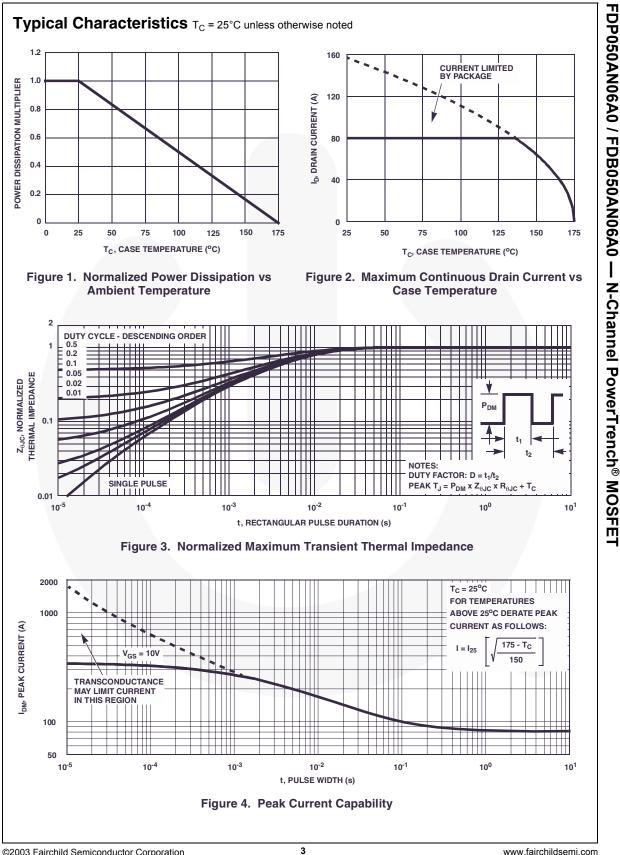


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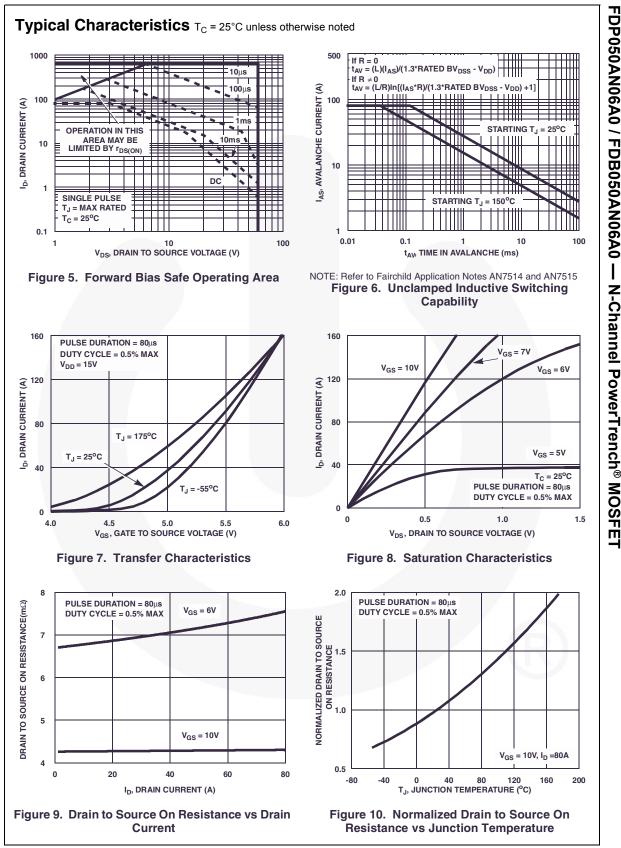
FDP050AN06A0 / FDB050AN06A0 — N-Channel PowerTrench[®] MOSFET October 2013

FAIRCHILD

Device Marking FDB050AN06A0		Device	Package	Reel Size 330 mm	Tape Width24 mm		Quantity 800 units		
		FDB050AN06A0	D ² -PAK						
FDP050AN06A0 FDP050AN06A0		TO-220	220 Tube		N/A		50 units		
Electric	al Char	acteristics T _C = 25°C	unless otherwise	e noted					
Symbol	Symbol Parameter		Test C	Conditions	Min	Тур	Max	Unit	
Off Chara	acteristic	S							
B _{VDSS}	Drain to S	Drain to Source Breakdown Voltage		I _D = 250μA, V _{GS} = 0V		-	-	V	
- 0033			$V_{DS} = 50V$	03	60 -	-	1		
IDSS	Zero Gate	Gate Voltage Drain Current	$V_{GS} = 0V$	T _C = 150 ^o C	-	-	250	μA	
I _{GSS}	Gate to Source Leakage Current		V _{GS} = ±20V		-	-	±100	nA	
	acteristic			0.50					
V _{GS(TH)}	Gate to Source Threshold Voltage		$V_{GS} = V_{DS}, I_{D}$		2	-	4	V	
r _{DS(ON)}			I _D = 80A, V _{GS} I _D = 40A, V _{GS}		-	0.0043	0.005	-	
	Drain to S	Drain to Source On Resistance		= 6V	-	0.007	0.011	Ω	
				I _D = 80A, V _{GS} = 10V, T _{.1} = 175 ^o C		0.0085	0.010		
			- 5			1			
	Characte	eristics							
CISS	Input Cap	Input Capacitance		a = 0	-	3900	-	pF	
C _{OSS}	Output Capacitance		─V _{DS} = 25V, V _{GS} = 0V, f = 1MHz		-	750	-	pF	
C _{RSS}		ransfer Capacitance			-	270	-	pF	
Q _{g(TOT)}		e Charge at 10V	$V_{GS} = 0V \text{ to } 1$			61	80	nC	
Q _{g(TH)}		Gate Charge	$V_{GS} = 0V \text{ to } 2$	V V _{DD} = 30V	-	8	11	nC	
Q _{gs}		ource Gate Charge	_	$I_{\rm D} = 80A$	-	24	-	nC	
Q _{gs2}	Gate Charge Threshold to Plateau		_	I _g = 1.0mA	-	16	-	nC	
Q _{gd}	Gate to D	rain "Miller" Charge			· ·	15	-	nC	
Switchin	g Charac	teristics (V _{GS} = 10V)							
t _{ON}	Turn-On Time				- 1	-	264	ns	
t _{d(ON)}	Turn-On Delay Time				-	16	-	ns	
t _r	Rise Time		$V_{DD} = 30V, I_D = 80A$ $V_{GS} = 10V, R_{GS} = 4.3\Omega$		-	160	-	ns	
t _{d(OFF)}	Turn-Off Delay Time				-	28	-	ns	
t _f	Fall Time					29	-	ns	
t _{OFF}	Turn-Off T	Turn-Off Time				-	86	ns	
Drain-So		le Characteristics	·						
Diam-50			- 20 4		-	1	1.05	V	
V _{SD}	Source to	Drain Diode Voltage	$I_{SD} = 80A$ $I_{SD} = 40A$		-	-	1.25 1.0	V	
	Reverse F	Recovery Time	I _{SD} = 40A I _{SD} = 75A, dI _{SD} /dt = 100A/μs		-	-	34	ns	
t		Recovered Charge	$I_{SD} = 75A$, $dI_{SD}/dt = 100A/\mu s$ $I_{SD} = 75A$, $dI_{SD}/dt = 100A/\mu s$		-	-	25	nC	
t _{rr} Q _{RR}	Reverse F			ιμαι ισυπνμο					

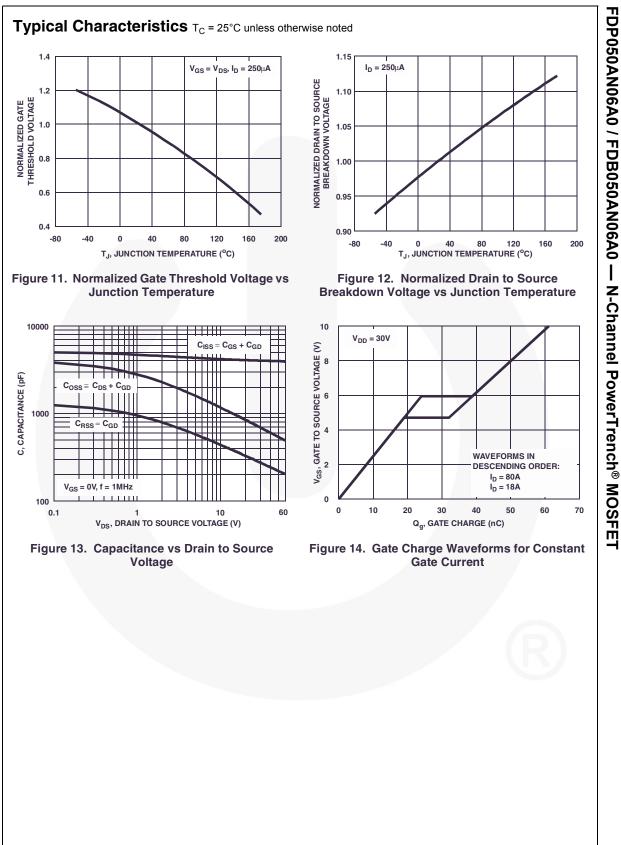


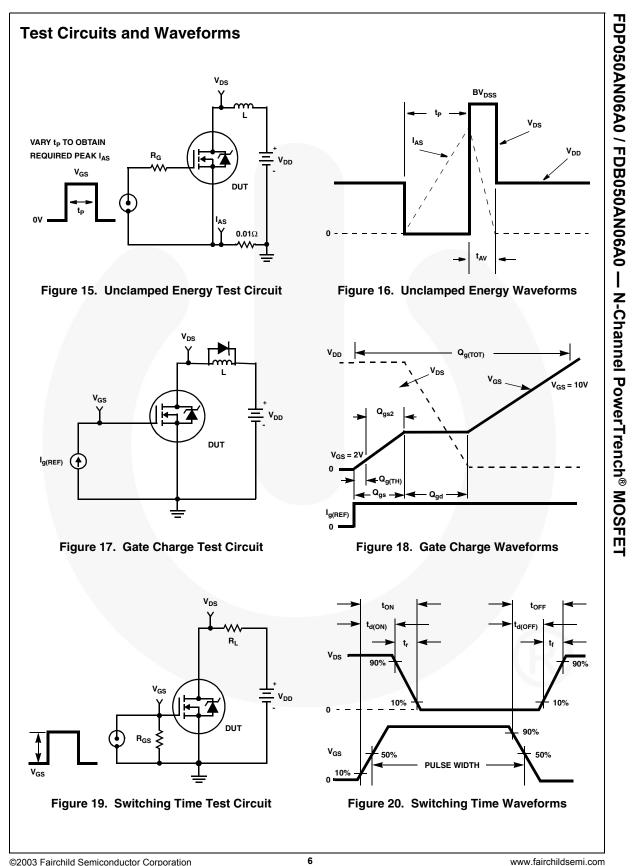
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Thermal Resistance vs. Mounting Pad Area

The maximum rated junction temperature, T_{JM} , and the thermal resistance of the heat dissipating path determines the maximum allowable device power dissipation, P_{DM} , in an application. Therefore the application's ambient temperature, T_A (°C), and thermal resistance $R_{\theta JA}$ (°C/W) must be reviewed to ensure that T_{JM} is never exceeded. Equation 1 mathematically represents the relationship and serves as the basis for establishing the rating of the part.

$$P_{DM} = \frac{(T_{JM} - T_A)}{R_{\theta JA}}$$
(EQ. 1)

In using surface mount devices such as the TO-263 package, the environment in which it is applied will have a significant influence on the part's current and maximum power dissipation ratings. Precise determination of P_{DM} is complex and influenced by many factors:

- Mounting pad area onto which the device is attached and whether there is copper on one side or both sides of the board.
- 2. The number of copper layers and the thickness of the board.
- 3. The use of external heat sinks.
- 4. The use of thermal vias.
- 5. Air flow and board orientation.
- 6. For non steady state applications, the pulse width, the duty cycle and the transient thermal response of the part, the board and the environment they are in.

Fairchild provides thermal information to assist the designer's preliminary application evaluation. Figure 21 defines the $R_{\theta,JA}$ for the device as a function of the top copper (component side) area. This is for a horizontally positioned FR-4 board with 1oz copper after 1000 seconds of steady state power with no air flow. This graph provides the necessary information for calculation of the steady state junction temperature or power dissipation. Pulse applications can be evaluated using the Fairchild device Spice thermal model or manually utilizing the normalized maximum transient thermal impedance curve.

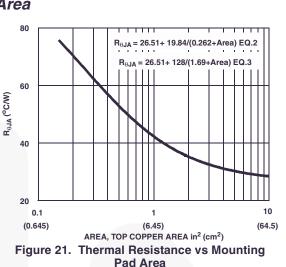
Thermal resistances corresponding to other copper areas can be obtained from Figure 21 or by calculation using Equation 2 or 3. Equation 2 is used for copper area defined in inches square and equation 3 is for area in centimeters square. The area, in square inches or square centimeters is the top copper area including the gate and source pads.

$$R_{\Theta JA} = 26.51 + \frac{19.84}{(0.262 + Area)}$$
(EQ. 2)

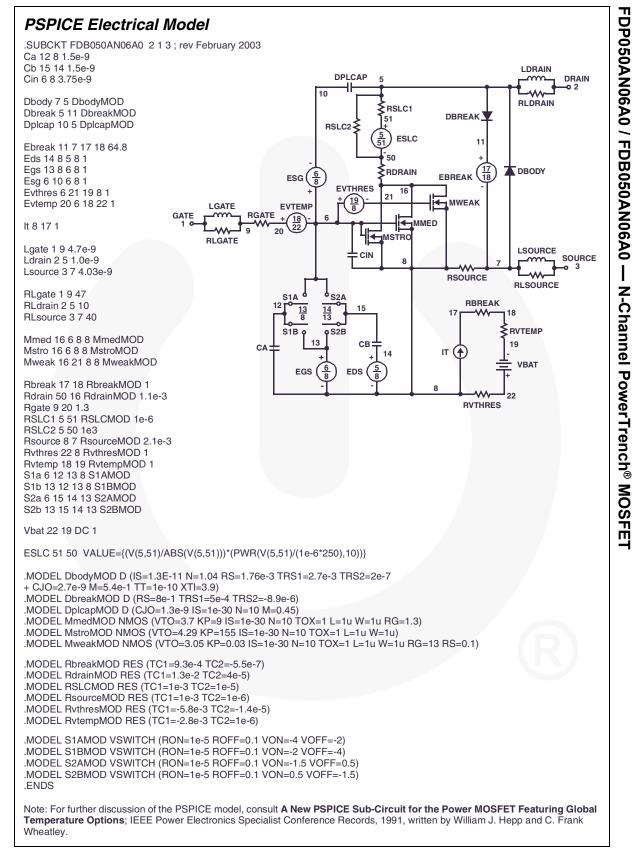
Area in Inches Squared

$$R_{\theta JA} = 26.51 + \frac{128}{(1.69 + Area)}$$
(EQ. 3)
Area in Centimeters Squared

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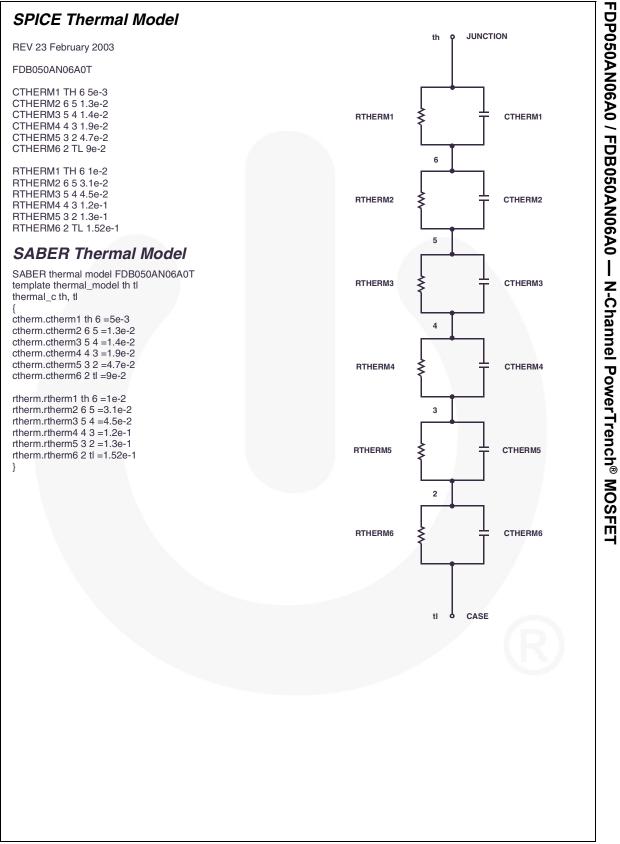
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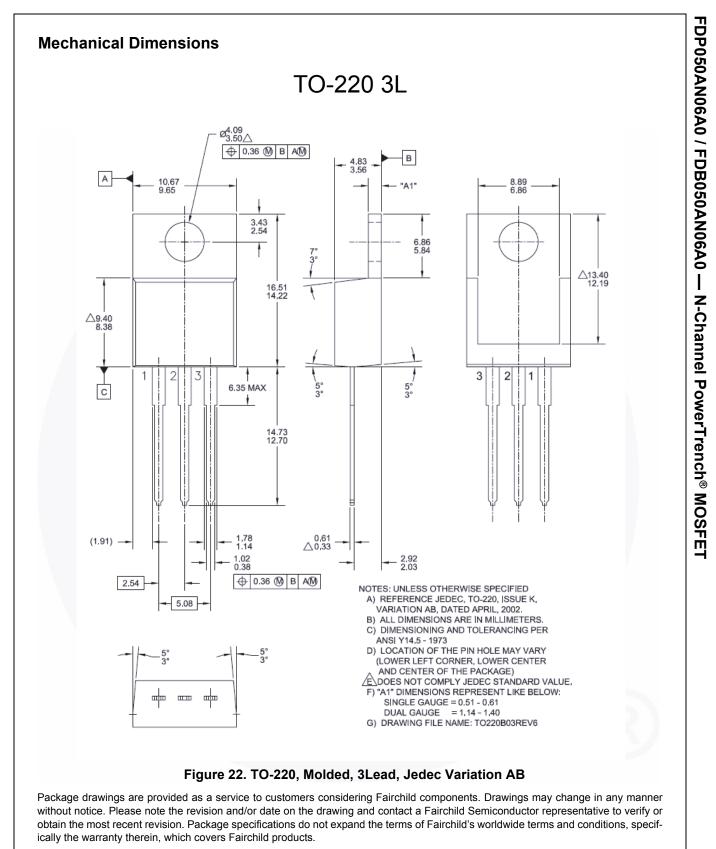


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SABER Electrical Model DP050AN06A0 / FDB050AN06A0 --rev February 2003 template FDB050AN06A0 n2,n1,n3 electrical n2,n1,n3 var i iscl dp..model dbodymod = (isl=1.3e-11,nl=1.04,rs=1.76e-3,trs1=2.7e-3,trs2=2e-7,cjo=2.7e-9,m=5.4e-1,tt=1e-10,xti=3.9) dp..model dbreakmod = (rs=8e-1,trs1=5e-4,trs2=-8.9e-6) dp..model dplcapmod = (cjo=1.3e-9,isl=10e-30,nl=10,m=0.45)m..model mmedmod = (type=_n,vto=3.7,kp=9,is=1e-30, tox=1) m..model mstrongmod = (type=_n,vto=4.29,kp=155,is=1e-30, tox=1) m..model mweakmod = (type=_n,vto=3.05,kp=0.03,is=1e-30, tox=1,rs=0.1) sw_vcsp..model s1amod = (ron=1e-5,roff=0.1,von=-4,voff=-2) DPLCAP DRAIN sw_vcsp..model s1bmod = (ron=1e-5,roff=0.1,von=-2,voff=-4) 02 10 sw_vcsp..model s2amod = (ron=1e-5,roff=0.1,von=-1.5,voff=0.5) RLDRAIN sw_vcsp..model s2bmod = (ron=1e-5,roff=0.1,von=0.5,voff=-1.5) **₹**RSLC1 c.ca n12 n8 = 1.5e-9 51 RSLC2 ₹ c.cb n15 n14 = 1.5e-9 ISCL c.cin n6 n8 = 3.75e-9 DBREAK 50 dp.dbody n7 n5 = model=dbodymod RDRAIN dp.dbreak n5 n11 = model=dbreakmod 6 ESG 11 dp.dplcap n10 n5 = model=dplcapmod EVTHRES 16 21 <u>19</u> 8 MWFAK LGATE spe.ebreak n11 n7 n17 n18 = 64.8 EVTEMP GATE RGATE ണ spe.eds n14 n8 n5 n8 = 1 18 22 EBREAK 9 20 spe.egs n13 n8 n6 n8 = 1 MSTR RLGATE spe.esg n6 n10 n6 n8 = 1 LSOURCE spe.evthres n6 n21 n19 n8 = 1 CIN SOURCE \mathbf{m} 8 spe.evtemp n20 n6 n18 n22 = 1 3 RSOURCE RLSOURCE i.it n8 n17 = 1 RBREAK I.lgate n1 n9 = 4.7e-9 13 17 \sim 18 I.ldrain n2 n5 = 1.0e-9 RVTEMP l.lsource n3 n7 = 4.03e-9 S1B S2B СВ 19 CA IT 14 res.rlgate n1 n9 = 47 VRAT res.rldrain n2 n5 = 105 EGS FDS res.rlsource n3 n7 = 40 8 22 m.mmed n16 n6 n8 n8 = model=mmedmod, l=1u, w=1u RVTHRES m.mstrong n16 n6 n8 n8 = model=mstrongmod, l=1u, w=1u m.mweak n16 n21 n8 n8 = model=mweakmod, l=1u, w=1u res.rbreak n17 n18 = 1, tc1=9.3e-4,tc2=-5.5e-7 res.rdrain n50 n16 = 1.1e-3, tc1=1.3e-2,tc2=4e-5 res.rgate n9 n20 = 1.3 res.rslc1 n5 n51 = 1e-6, tc1=1e-3,tc2=1e-5 res.rslc2 n5 n50 = 1e3res.rsource n8 n7 = 2.1e-3, tc1=1e-3,tc2=1e-6 res.rvthres n22 n8 = 1, tc1=-5.8e-3,tc2=-1.4e-5 res.rvtemp n18 n19 = 1, tc1=-2.8e-3,tc2=1e-6 sw_vcsp.s1a n6 n12 n13 n8 = model=s1amod sw_vcsp.s1b n13 n12 n13 n8 = model=s1bmod sw_vcsp.s2a n6 n15 n14 n13 = model=s2amod sw_vcsp.s2b n13 n15 n14 n13 = model=s2bmod v.vbat n22 n19 = dc=1 equations { i (n51->n50) +=iscl iscl: v(n51,n50) = ((v(n5,n51)/(1e-9+abs(v(n5,n51))))*((abs(v(n5,n51)*1e6/250))** 10)) }

N-Channel PowerTrench® MOSFET

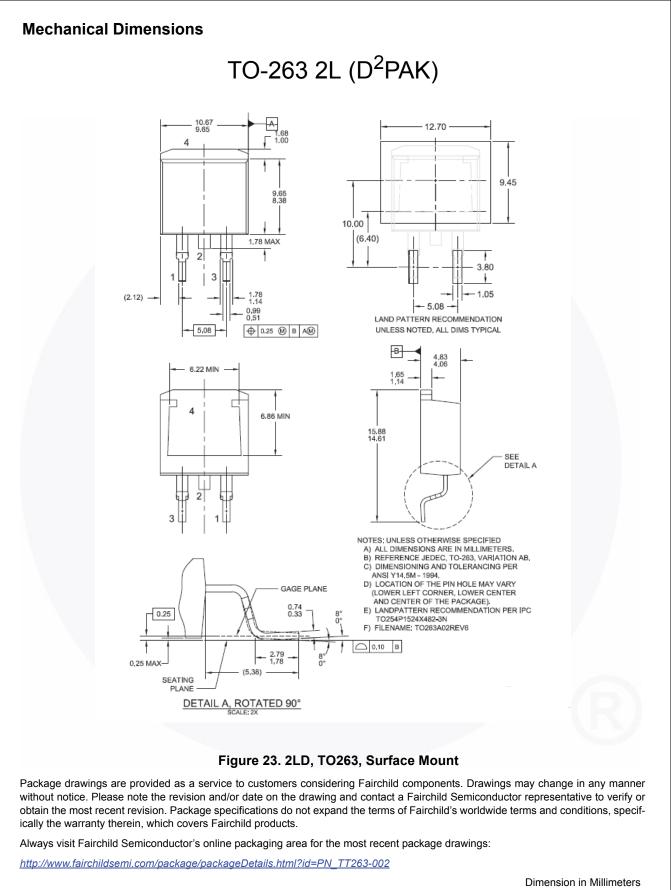




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Dimension in Millimeters





No Identification Needed

Obsolete

Full Production

Not In Production

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